

# EFRC Training Workshop

## Lubrication and Wear

Cylinder lubrication,  
Effect on wear of pistons and rider rings

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# CONTENT:

1. Cylinder lubrication
2. Wear
3. Field experience



# CONTENT:

## 1. Cylinder lubrication

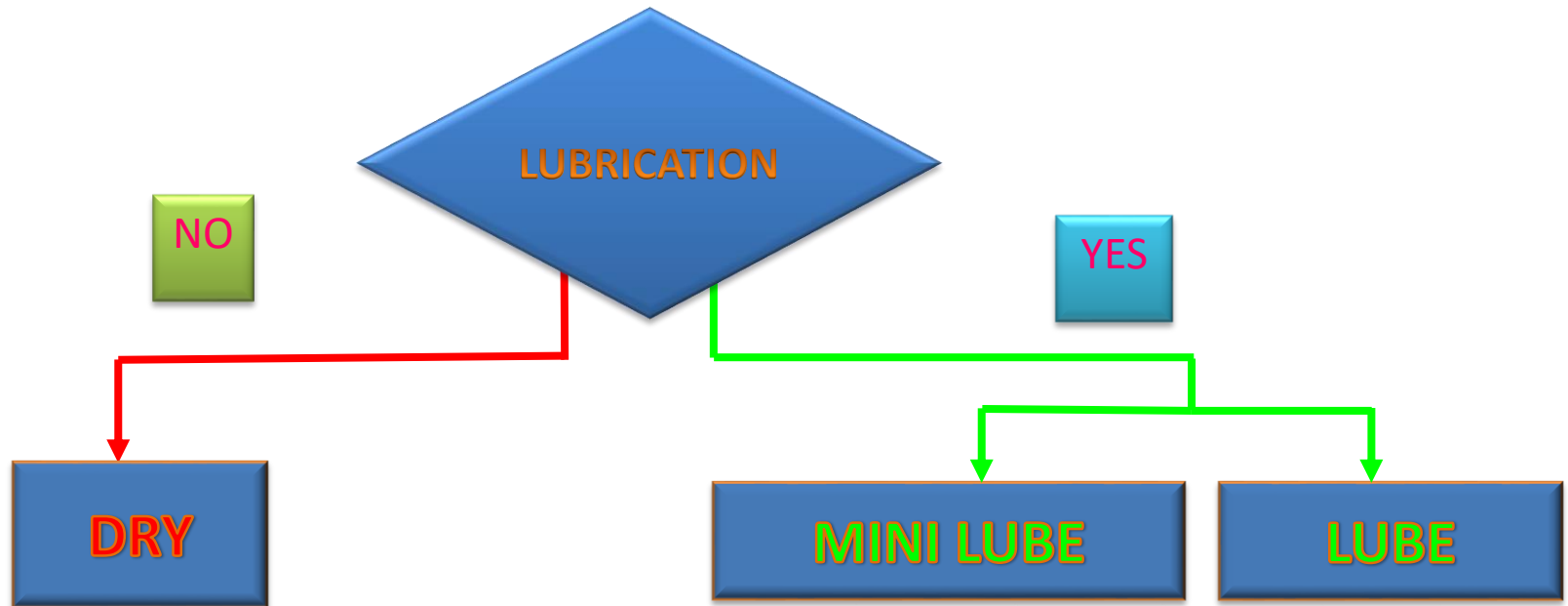
- Options
- Purposes
- Oils
- Quills
- Lubrication systems

## 2. Wear

## 3. Field experience



# CYLINDER LUBRICATION: OPTIONS



Depending on:

- ✓ Lubrication tolerability
- ✓ Economic evaluation
- ✓ Requested reliability
- ✓ Discharge pressure



# CYLINDER LUBRICATION: PURPOSES

## Purposes

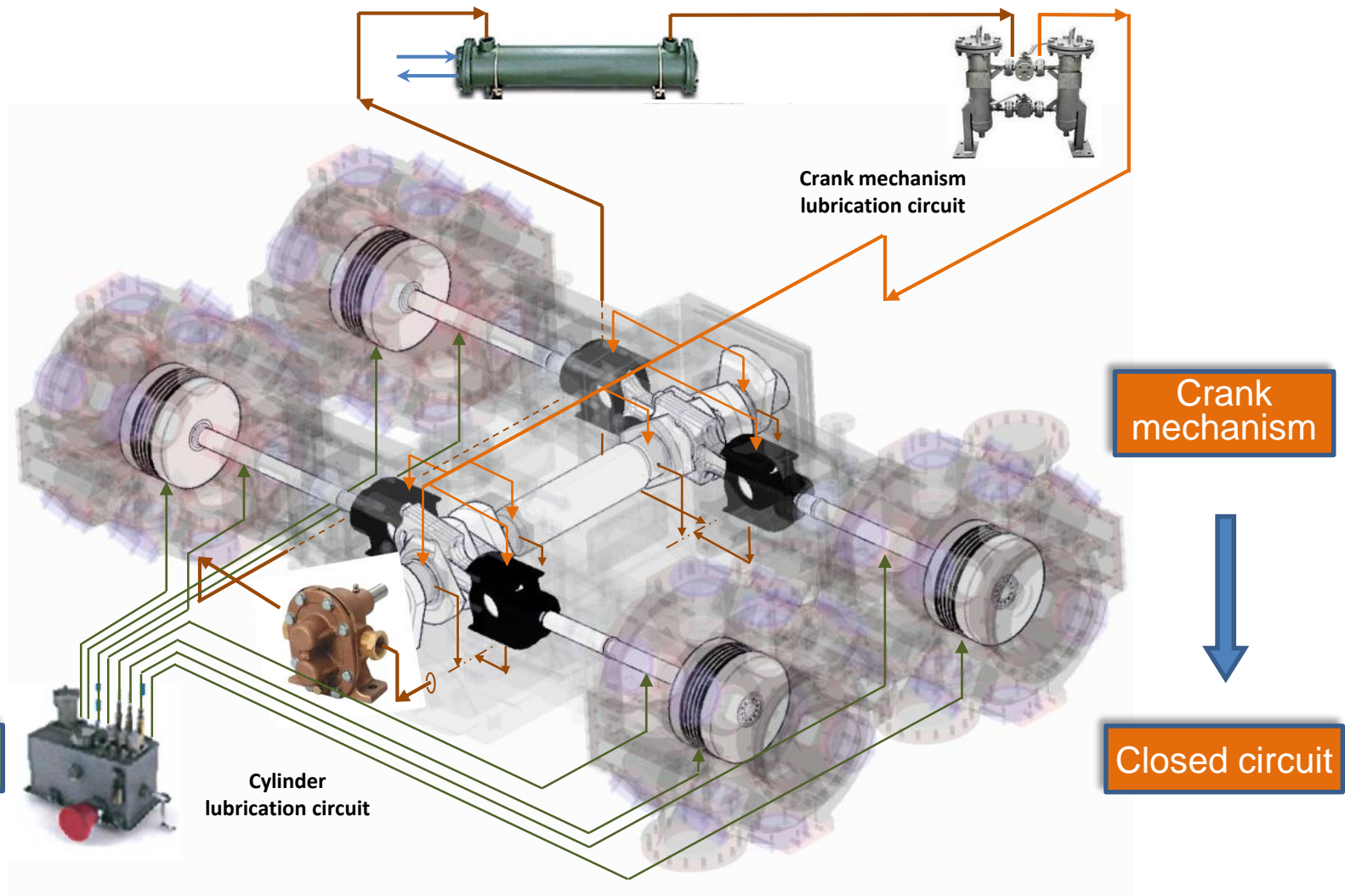
- ✓ Minimize wear
- ✓ Dissipate frictional heat
- ✓ Remove impurities
- ✓ Protect metal parts from corrosion

## Characteristics

- ✓ High pressure working conditions
- ✓ Low (*drops/min*), measured and constant flow rate required
  - as lube oil is a contaminant for the process gas
  - to guarantee controlled flow for each injection point
- ✓ The lube oil cannot be recovered
- ✓ Heat dissipation



# CYLINDER AND CRANK MECHANISM LUBE CIRCUITS



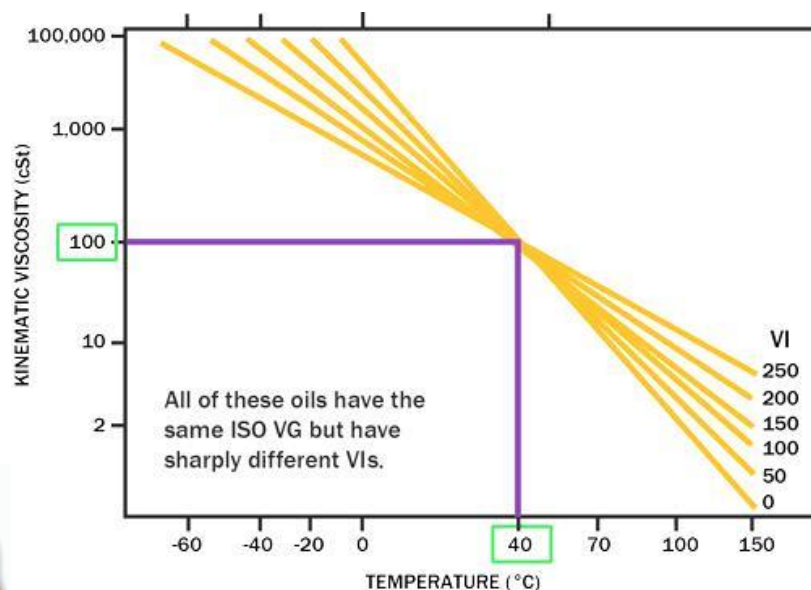
# TYPICAL LUBRICATION OILS FOR CYLINDERS

Compressor oil viscosity generally used for cylinders: ISO VG 220 (ISO3448)  
ISO VG 320

Necessary to know how the viscosity changes in relation to a temperature change

**ISO viscosity grade only refers to the viscosity at the temperature of 40 °C**

**Viscosity Index (VI)** = variation of viscosity with temperature

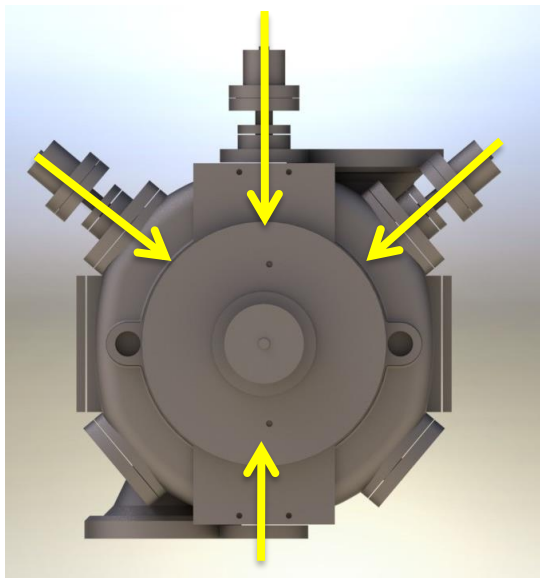


The higher is the V.I., the lower is the change of viscosity at the same  $\Delta$  temp.

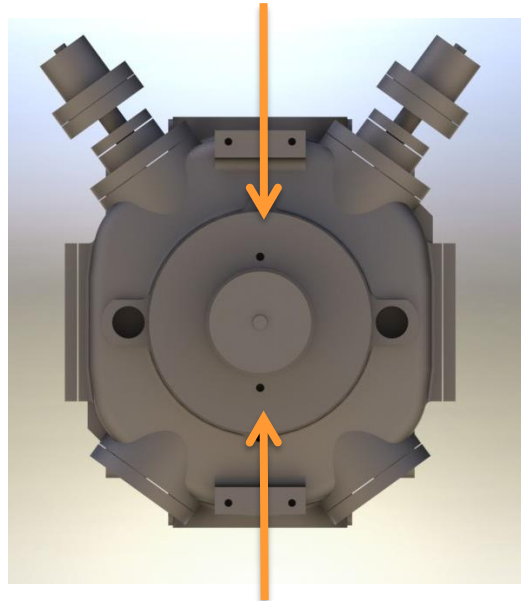


# CYLINDER LUBRICATION INJECTION POINTS

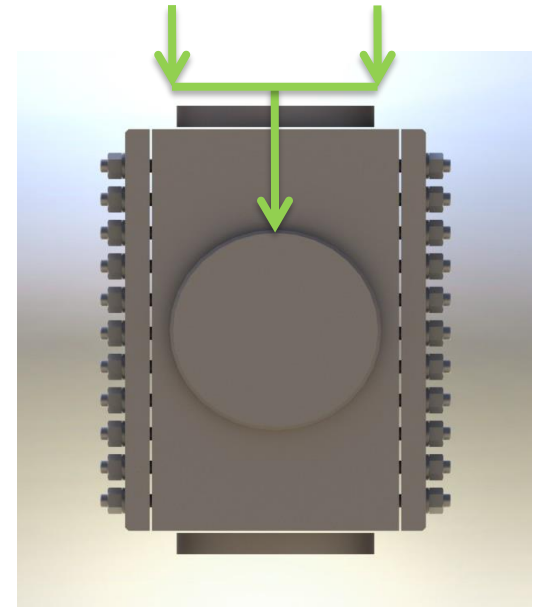
The oil must be distributed in all the area swept by the piston



Large cylinder



Small cylinder

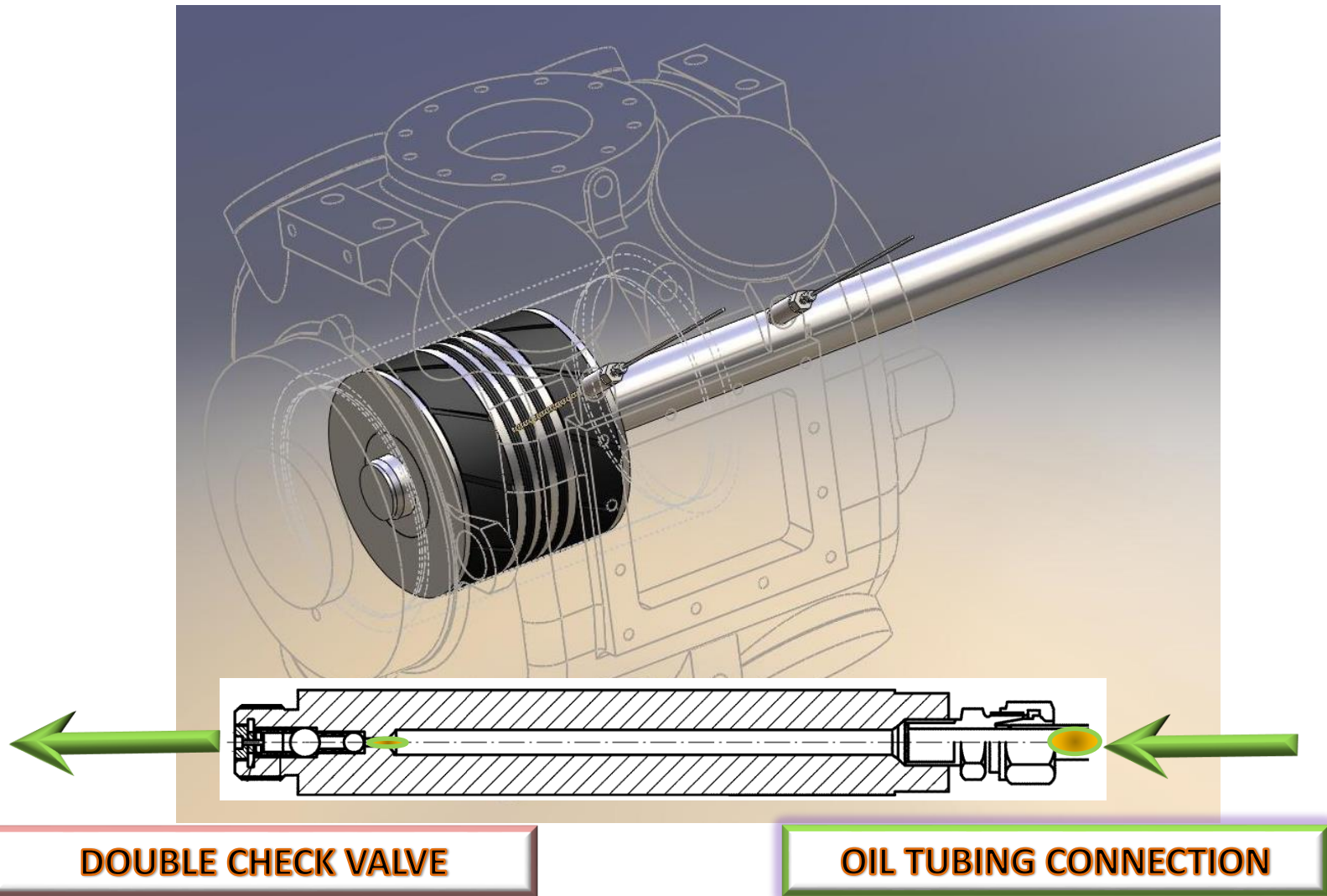


Forged small cylinder





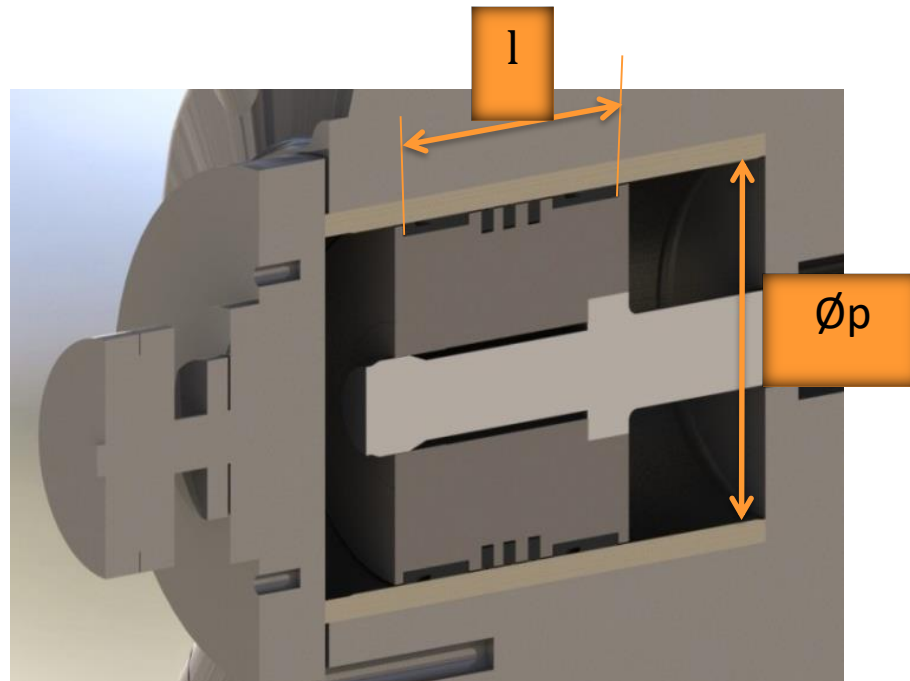
# LUBRICATION QUILLS



# OIL CONSUMPTION

**Cylinder** theoretical consumption =  $C_x \cdot SS_p$

- $C_x$  = constant specific consumption, depending on the Mfr experience
- $SS_p$  = piston Swept Surface



The API618 requires a lubrication system capable of providing oil flow rates between 75% and 200% of the nominal flow

# OIL CLASSIFICATION

APPLICATION	TYPE	MAIN CHARACTERISTICS
• Low pressure gas	Mineral or synthetic	Low tendency to foam formation
• High humidity gas	Mineral or synthetic	Antioxidant properties, washing resistance
• Solvents or condensable gases	Mineral or synthetic	low emulsion time, film strength
• Low inlet temperature	Mineral or synthetic	Low pour point
• Air	Mineral or synthetic	Low emulsion time
• Ethylene (LDPE)	Synthetic	Antioxidant, corrosion-protecting qualities, usable for packaging food, low viscosity index

**Lube oil selection shall be a compromise between lubricating properties and process**

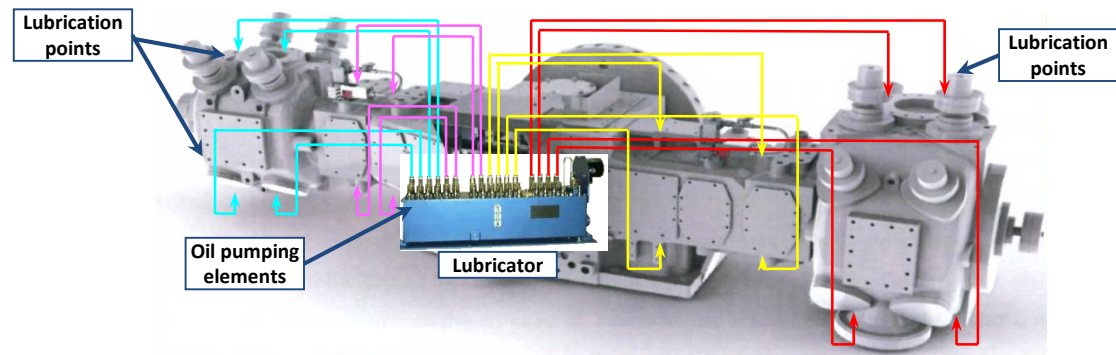


# CYLINDER LUBRICATION SYSTEMS

✓ **PtP** System  
(Pump-to-Point)



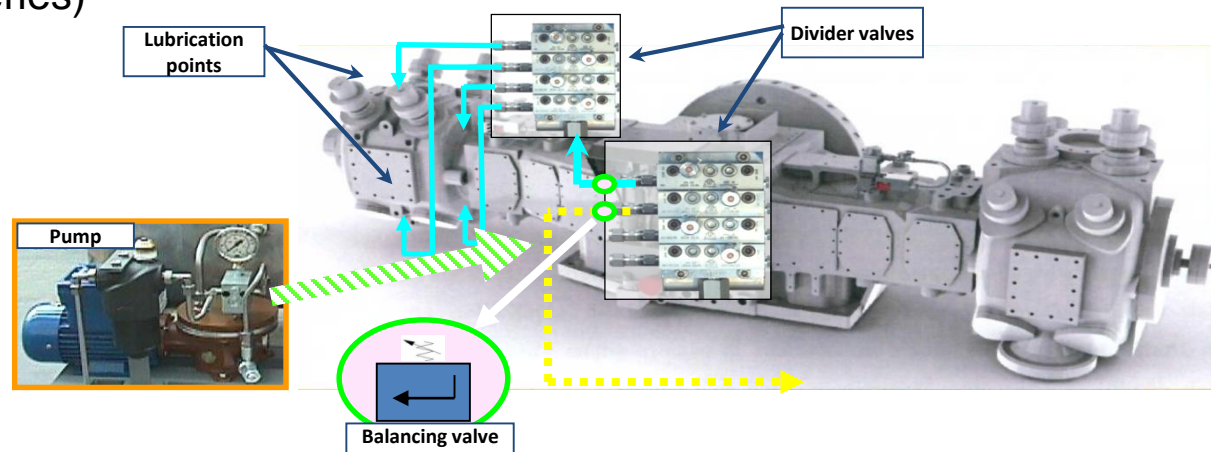
A single pumping element for each lubrication point



✓ **PS** System  
(Progressive Series)



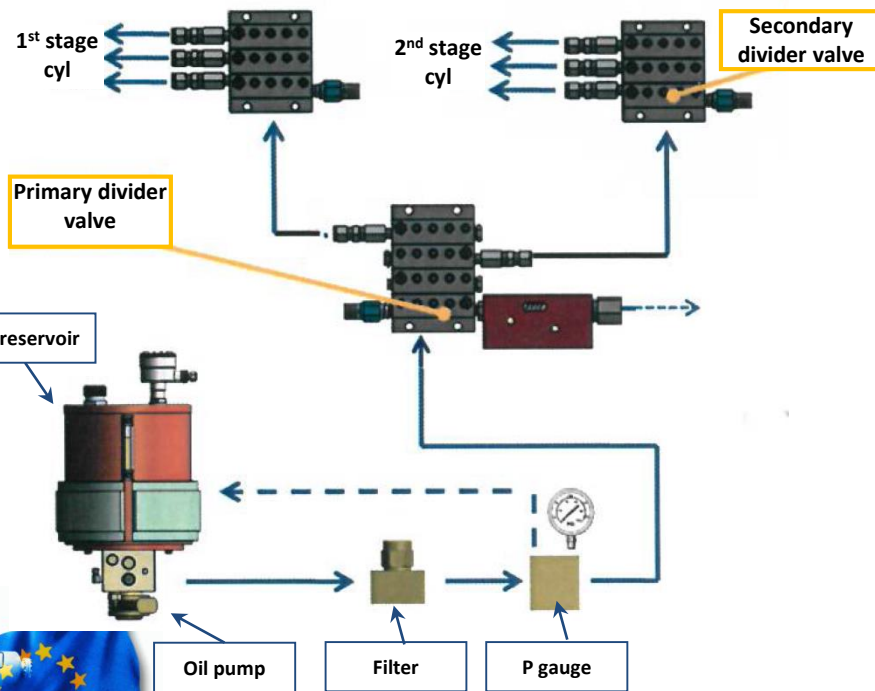
A pumping element with Divider Valves



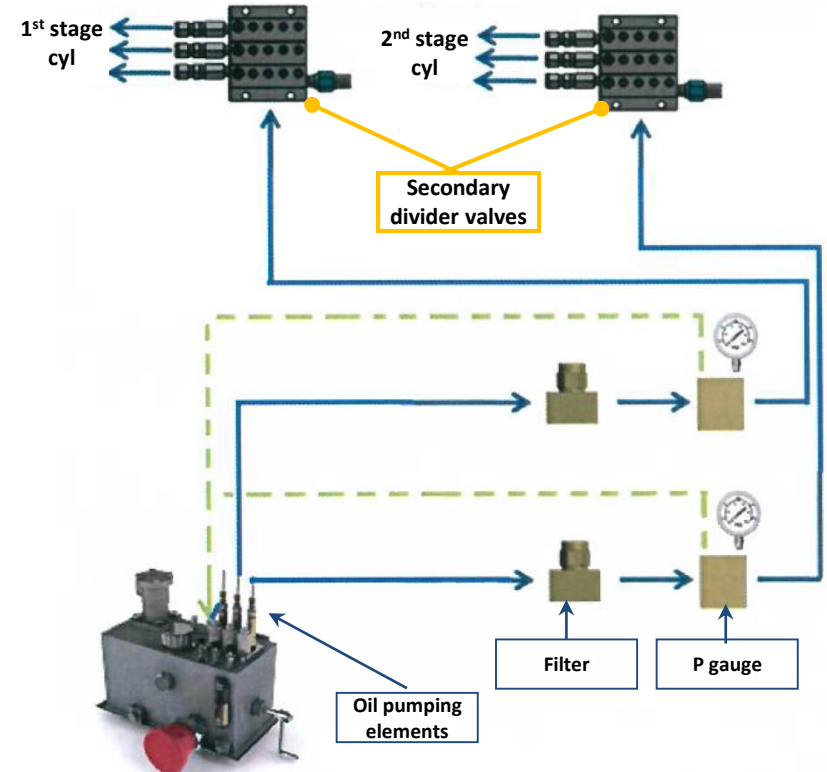
# CYLINDER LUBRICATION SYSTEMS

## PS lubrication systems

Traditional version  
with primary and secondary  
Divider Valves



Hybrid version  
with secondary  
Divider Valves only



## COMPARISON

PtP System	Traditional PS System	Hybrid PS System
<b>PROS:</b>	<b>PROS:</b>	<b>PROS:</b>
✓ High injection frequency	✓ Only one pumping unit	✓ Few pumping elements with optimum operating range
✓ Flow rate to the single point: <ul style="list-style-type: none"> <li>• independent from the other points</li> <li>• easily adjustable</li> </ul>	✓ Oil flow rate matching requirements	✓ Each pumping elements feeds the full flow required by one cylinder/stage
✓ No additional device downstream of the pumping elements	✓ Easier flow monitoring	✓ The flow rate can be easily adjusted to each cylinder /stage
		✓ Balancing valves not necessary
		✓ Oil consumption minimized
<b>CONS:</b>	<b>CONS:</b>	<b>CONS:</b>
✓ Flow rate higher than necessary <ul style="list-style-type: none"> <li>• Setting to minimal flow rate</li> <li>• Unstable operating conditions</li> <li>• Oil consumption may result higher than necessary</li> </ul>	✓ Flow rate to each single point not adjustable	✓ In the event of blockage of a line the divider valve makes all the relative cylinders run dry
	✓ If a line is blocked, the secondary divider valve stops, stopping also the primary one and making all the cylinders run dry	
	✓ Balancing valves required	



# CONTENT:

1. Cylinder lubrication
2. **Wear**
3. Field experience





# CONTENT:

## 1. Cylinder lubrication

## 2. Wear

- Definition and possible causes
- Wear rate
- API 618 prescription
- Piston rings and rider rings
- Materials

## 3. Field experience





# WEAR: DEFINITION AND ORIGIN

**Wear:** Is the loss of surface material that occurs progressively on the surfaces of bodies in contact when subject to relative movement

## Reasons for rapid wear of cylinder seals and counterparts:

- ✓ Inappropriate lubricant oil quality and/or quantity
- ✓ Wrong number /design of sealing elements
- ✓ Too high surface pressure on rider rings
- ✓ Wrong sliding parts material selection
- ✓ Abrasive particles / solvents in the process gas
- ✓ Wrong roughness of sliding surfaces



# WEAR RATE

General relationship of wear rate ( $W_r$ ):

$$W_r = kPVT$$

Where:

- k** = function of material
- P** = contact pressure (variable during each piston stroke for seal rings)
- V** = piston velocity (variable during each piston stroke)
- T** = time (service life)

**Wear rate ( $W_r$ ) is proportional to friction**



# API 618 PRESCRIPTION ON RIDER RINGS

From point 6.10.3.2 of API 618 5<sup>th</sup> Edition:

For non-lubricated horizontal cylinders, the bearing load calculated from Equation 2 on nonmetallic wear bands shall not exceed 0.035 N/mm<sup>2</sup> (5 lbf/in.<sup>2</sup>) based on the mass of the entire piston assembly plus half the mass of the rod divided by the projected area of a 120° arc of all wear bands (see Equation 2).

For lubricated horizontal cylinders, the bearing load calculated from Equation 2 on wear bands, if used, shall not exceed 0.07 N/mm<sup>2</sup> (10.0 lbf/in.<sup>2</sup>) using the same approach described for nonmetallic wear bands.

$$L_B = \frac{M_{PA} + (M_R/2)}{(0.866 \times D \times W)} \quad (2)$$

Where:

$L_B$  is the bearing load on wear band in N/mm<sup>2</sup> (lbf/in.<sup>2</sup>);

$M_{PA}$  is the weight of piston assembly in N (lbf);

$M_R$  is the weight of piston rod in N (lbf);

$D$  is the cylinder bore diameter in mm (in.);

$W$  is the total width of all wear bands in mm (in.).

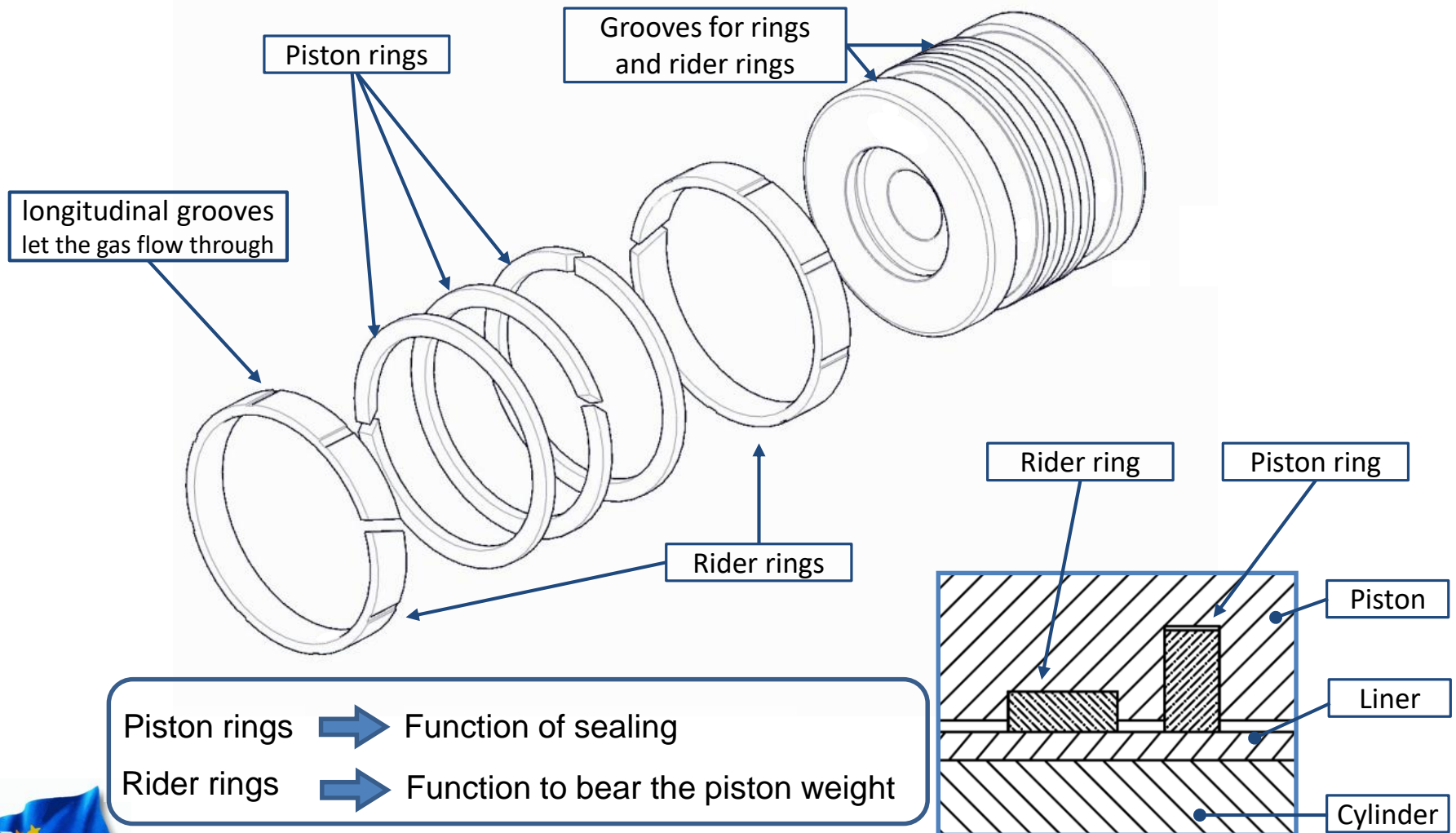
Max specific load:

**0.07 N/mm<sup>2</sup>** ➡ **lubricated service**

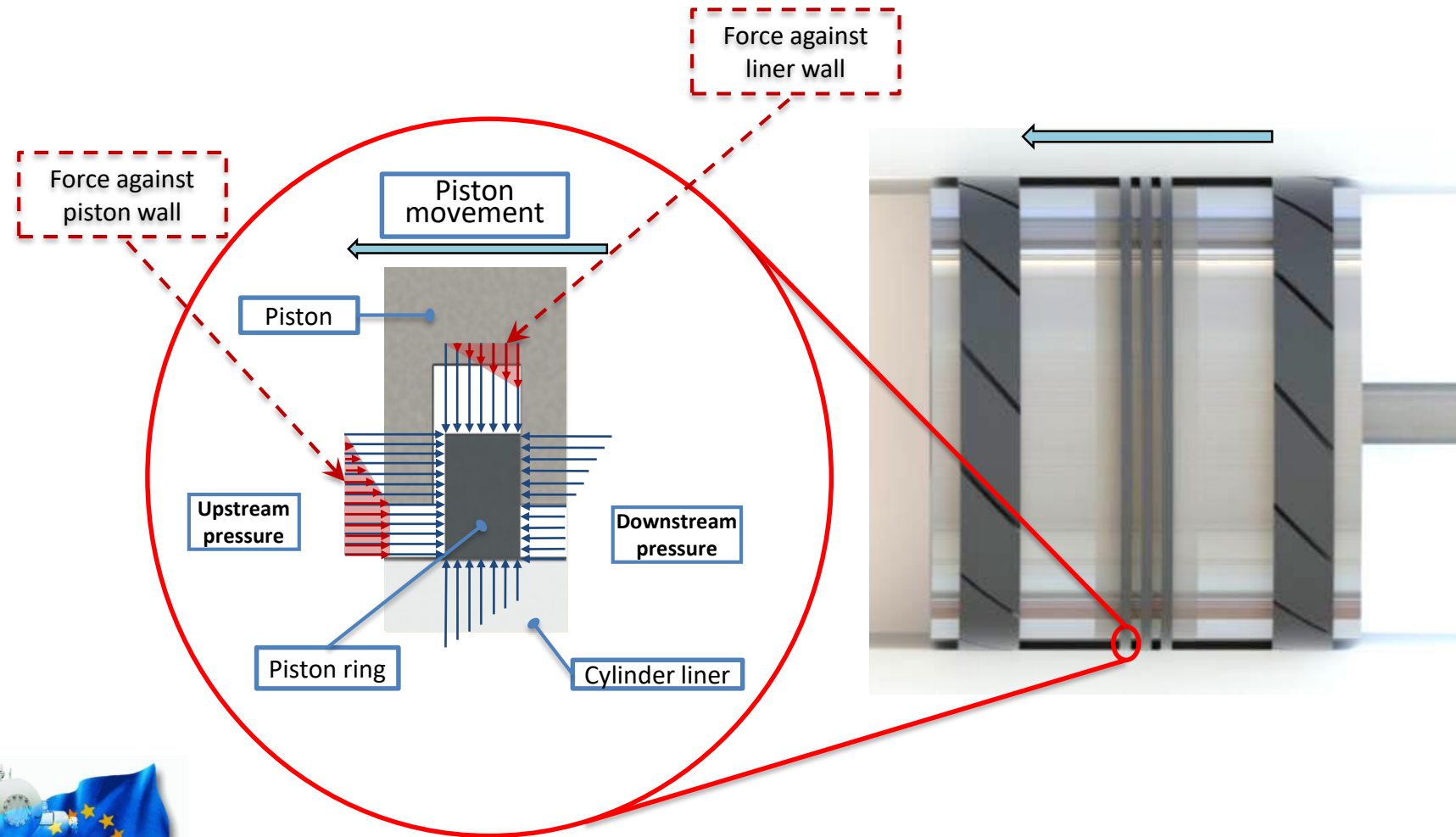
**0.035 N/mm<sup>2</sup>** ➡ **dry service**



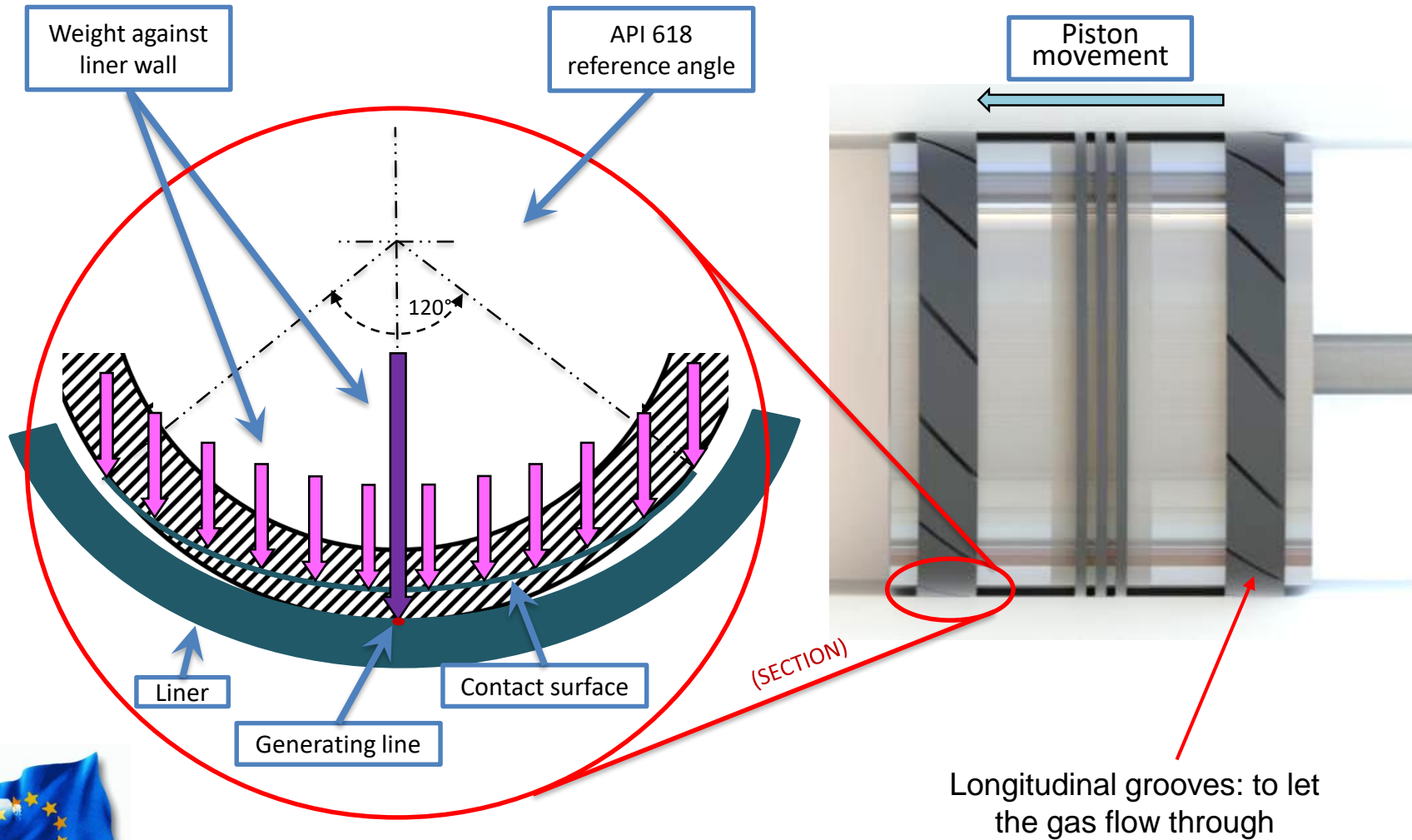
# PISTON RINGS AND RIDER RINGS



# HOW DO PISTON RINGS WORK



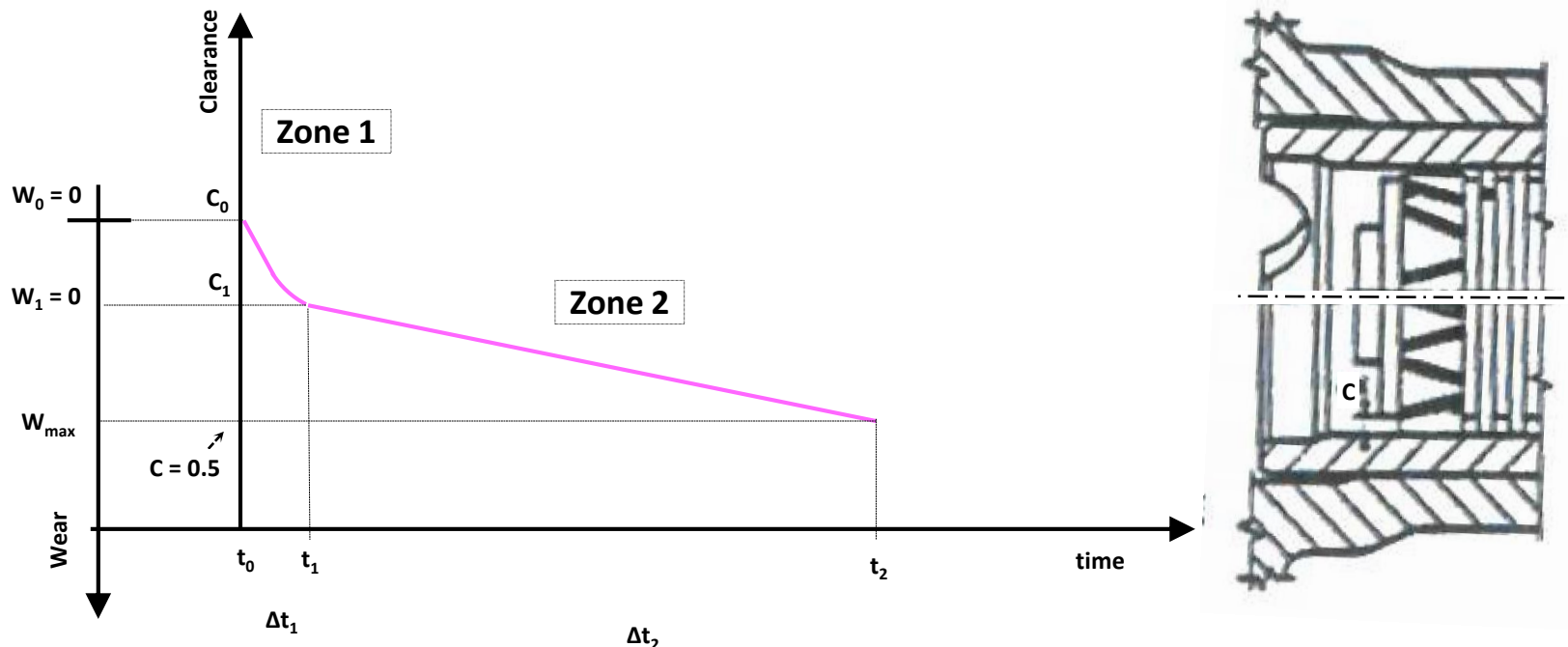
# HOW DO RIDER RINGS WORK



# RIDER RINGS WEAR

## Typical wear pattern

- Zone 1:** The contact zone changes from a generatrix to a wider surface → High wear rate
- Zone 2:** The wear rate stabilizes to a much lower value → Stable low wear rate



Clearance C shall be monitored -  $C_{min}$  value: ~ 0.5 mm

# THERMOPLASTIC MATERIALS

## Main features to be achieved

Low coefficient of friction	➡	to limit heating and wear of the counter parts
Good thermal conductivity	➡	to assist dispersion of generated heat
High mechanical resistance	➡	to withstand the $\Delta P$ to which the parts are submitted

## Main filler goals

- ✓ To increase resistance to wear
- ✓ Increases thermal conductivity
- ✓ Improves of mechanical characteristics

## Surface finishing

Balance between too rough and too smooth  
Optimal finishing of cylinder liner: 0.3-0.4  $\mu\text{m}$  Ra

After a first period of thermoplastic material transfer,  
sliding takes place between two surfaces both having a low coefficient of friction





# CONTENT:

1. Cylinder lubrication
2. Wear
3. **Field experience**



# FIELD EXPERIENCE

## Description of the system

Compressor Type	Reciprocating Compressor
Service	Heavy hydrocarbons (sour gas with H <sub>2</sub> S presence)
Compressor design	4 cyl.s, balanced opposed
Nr of cylinders / stages	2 / 2
Lubricated	Yes
Driver	Electric motor
Transmission type	elastic coupling
Nameplate Power	835 kW
Suction /Discharge Pressure	1.0 / 6.0 bara
Piston rings/rider rings mtl	PTFE

### Problem

Rapid wear of piston rings and rider rings  
(of a 2<sup>nd</sup> stage cylinder at 2 months by 1<sup>st</sup> start)



### Early action

Rings/wear bands replaced with PTFE differently filled  
Wear bands with different design



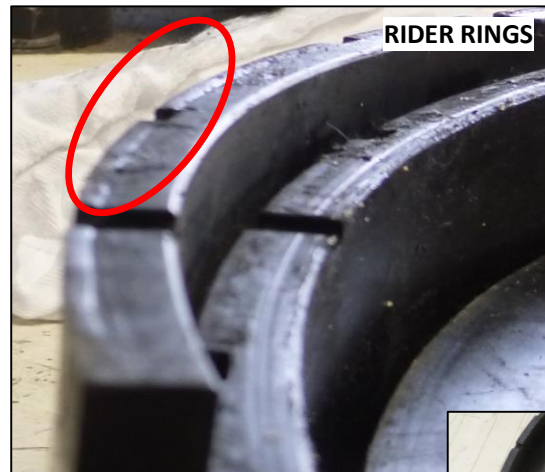
# FIELD EXPERIENCE

## Description of the problem: sight findings

- ✓ Cylinders found dry;
- ✓ Solid, non metallic particles covered the piston head; ➡



- ✓ Rider rings extruded; ➡



- ✓ Rider rings bent; ➡



# FIELD EXPERIENCE

## Description of the problem: measurements carried out

### ✓ Lubrication:

measured values lower than the nominal values

point of lubrication	outlets per cyl./packing	flow rate per outlet (drops/min)	
		nominal	measured
cylinder 1, 3 (1st stage)	1 / 1	11	6
cylinder 2, 4 (2nd stage)	1 / 1	7	6
packing boxes, cylinder 1, 3	1 / 1	5	3
packing boxes, cylinder 2, 4	1 / 1	5	3

### ✓ Gas and walls temp.s verification:

lower temperatures on cyl with new rings/rider rings

	gas temp	upper wall temp	lower wall temp
suction	60 °C	---	---
discharge	105 °C		
cyl#4 (new rings)	---	110 °C	120 °C
cyl#2 (original rings)	---	120 °C	130 °C

### ✓ Cylinders dimensions:

discrepancies between nominal and measured dimensions:

	Nominal dimension [mm]	Measured dimension [mm]
1 <sup>st</sup> stg wear band length	49.25	49.40
2 <sup>nd</sup> stg wear band length	68.95	69.40



# FIELD EXPERIENCE

## Diagnosis:

- ✓ Lubrication system failure:
  - very low oil flow;
  - intermittent lubrication: not good for PTFE;



## Suggested solution:

New lubrication system: progressive type

- increased oil quantity:
- More reliable lube system;
- each injection point monitored;

	<u>measured:</u>	<u>necessary:</u>
1 <sup>st</sup> stage	6 drops/min	50 drops/min
2 <sup>nd</sup> stage	6 drops/min	25 drops/min

- ✓ PTFE seals can be penalized by:
  - gas condensation (due to heavy hydroc.s)
  - presence of particles in the gas



Rings changed from PTFE to PEEK as more resistant:

- to condensate;
- to particles;

- ✓ Rise in wall temperature



Rings/wear bands design changed:

- more longitudinal grooves for rider rings;
- lower expansion coefficient

- ✓ Measured dimensions on rings / wear bands not matching the nominal ones



New piston design:

- longer rider rings to reduce the specific pressure
- larger clearances for seals

- ✓ Rod drop monitoring unreliable



Correct monitoring system



# CONCLUSION

## Wear causes:

- ✓ Mainly:
  - Lubrication system (type and quantity)
- ✓ Besides:
  - Materials of ring seals and rider rings
  - Shape of the rider rings
  - Correct dimensioning of rings grooves
  - Heat dissipation
  - Roughness of the sliding surfaces
  - Rod drop monitoring

## Notes:

- ✓ Several aspects may con-cause the wear of rings and rider rings
- ✓ When present, **the reliability of the lubrication system is fundamental**
- ✓ The worst running conditions for PTFE seals is **intermittent** lubrication



# Questions

